

# Multi-Contact Whole-Body Force Control for Position-Controlled Robots

Quentin Rouxel, Serena Ivaldi, Jean-Baptiste Mouret

Inria, Université de Lorraine, CNRS, Loria, F-54000.



https://hucebot.github.io/seiko\_controller\_website/



#### Multi-Contact on Position-Controlled Robots



 Multi-contact tasks require realizing specific contact

# Equilibrium Equation and Flexibility Model

Assumption: quasi-static equilibrium

Whole-body equilibrium equation: L $g(q) = S \tau + J(q)^{\mathsf{T}} \lambda$ Elastic joint flexibility model: $\tau^{\mathsf{flex}} = K(\theta^{\mathsf{cmd}} - \theta^{\mathsf{flex}})$ 

Linearization of the equilibrium equation:

 $\boldsymbol{g}(\boldsymbol{q}) + \frac{\partial \boldsymbol{g}}{\partial \boldsymbol{q}} \Delta \boldsymbol{q} = \boldsymbol{S} \boldsymbol{\tau} + \boldsymbol{S} \Delta \boldsymbol{\tau} + \boldsymbol{J}(\boldsymbol{q})^{\mathsf{T}} \boldsymbol{\lambda} + \boldsymbol{J}(\boldsymbol{q})^{\mathsf{T}} \Delta \boldsymbol{\lambda} + \left(\frac{\partial \boldsymbol{J}^{\mathsf{T}}}{\partial \boldsymbol{q}}^{\mathsf{T}} \boldsymbol{\lambda}\right) \Delta \boldsymbol{q}$ Feedback law over measured contact forces:

 $\Delta \boldsymbol{\lambda}^{\mathsf{effort}} = \Delta \boldsymbol{\lambda}^{\mathsf{d}} + K_p(\boldsymbol{\lambda}^{\mathsf{d}} - \tilde{\boldsymbol{\lambda}}^{\mathsf{read}}) - K_d \dot{\boldsymbol{\lambda}}^{\mathsf{read}}$ 

# Experiments on Talos Humanoid Robot



- force distribution
- Redundancy in force
   distribution: one posture,
   multiple force distributions

Position-controlled robots are still widespread and are more robust to model errors than torque-controlled
But position-controlled robots cannot directly control contact forces

**Problem:** How to control contact force on position controlled robot?

#### Main Ideas

- Real systems always have internal flexibilities/impedance
- With flexibilities, force distribution is uniquely defined
- Flexibilities are unobservable, but can be predicted with nonlinear whole-body optimization
- For a given joint position command, the whole-body configuration is unique and well defined
- Joint position commands are optimized to get desired contact forces given flexibilities

## SEIKO: Sequential Equilibrium Inverse Kinematic Optimization



Teleoperated multi-contact motions: traversal of sloped uneven ground with wall contact (left), stepping up 15 cm with enhanced stability (middle), and hand contact extending reaching distance (right)



#### Tracking of hand contact force during pushing task (left), and smooth contact switching (right)



Far reach with and without unmodeled load (left), and damping effect over torso oscillations (right)

#### Robustness Against Motion Speed and Model Error

- Whole-Body admittance controller using two Sequential Quadratic Program optimizations
- Input: Cartesian command for each effector (position and/or velocity) + contact switch trigger
- **Output**: corrected joint position commands realizing desired posture and contact forces
- SEIKO Retargeting: computes feasible desired whole-body configurations from commands
- SEIKO Controller: updates joint position command to indirectly regulate forces exploiting flexibilities

QP Formulations		
SEIKO Retargeting	SEIKO Controller	
<ul> <li>Inputs: target pose and contact state for each effector</li> </ul>	<ul> <li>Inputs: measured contact forces, desired whole-body configuration</li> </ul>	
<ul> <li>Solve for: desired joint position, contact force, joint torque</li> <li>Objectives: reach target effector pose and minimize joint torque</li> <li>Constraints: balance, contact stability, joint</li> </ul>	<ul> <li>Solve for: corrected joint position, predicted joint position, torque and contact forces under flexibility deflections</li> <li>Objectives: regulate contact forces</li> <li>Constraints: balance, joint kinematic and torque</li> </ul>	
kinematic and torque limits	limits	



• Number of successful trials without fall (out of 10) of reaching motions near feasibility boundary

- Varying hand velocity (2 cm/s to 40 cm/s) and added hand mass (none to 12 kg)
- Compare without the SEIKO Controller (left), with the SEIKO Controller but without considering joint torque limits (middle), and using the full control method (right)

## References

- [1] Q. Rouxel et al. "Multicontact motion retargeting using whole-body optimization of full kinematics and sequential force equilibrium". In: *IEEE/ASME T-MECH* (2022).
- [2] R. Wen et al. "Collaborative Bimanual Manipulation Using Optimal Motion Adaptation and Interaction Control Retargetting Human Commands to Feasible Robot Control References". In: *IEEE RAM* (2023).

	SEIKO Retargeting:	SEIKO Controller:	
	from operator's Cartesian commands	measured errors and joint flexibility model $ extsf{ heta}^{ extsf{cmd}}$ Flexible Configuration $ extsf{ heta}^{ extsf{cmd}},  extsf{ heta}^{ extsf{flex}},  extsf{ heta}^{ extsf{flex}}$	
Quitabing	Contact State and	$\Delta \lambda^d$	Joint Position









